# AN INTRODUCTION TO AGC CONTROLLED INTERCONNECTED UNEQUAL AREAS

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Abstract: - This paper manages programmed age control (AGC) of an interconnected two region inconsistent warm framework. Execution of ordinary PID regulator is contrasted and recently present altered traditional regulator named as PID1 and PID2 regulator. The exhibition of the proposed regulator has been assessed, which gives better powerful reaction then the customary PID regulator over wide scope of working condition and framework boundary varieties.

Keywords:- Automatic Generation Control, Structure1 and2 Proportional plus Integral Plus Derivative Controller (PID 1 & PID 2).

# 1. INTRODUCTION

The principle goals of programmed age control are to direct framework recurrence inside adequate reach and to keep up with the trade of force between control regions as close as conceivable the timetable worth by changing the result of chosen generator. The power framework loads are exceptionally delicate to recurrence. Any abrupt burden change in a control space of an interconnected power framework will prompt recurrence deviation just as tie-line power deviation [1].

L.C. Saika, S. Debbarama, M. Pathak,[2].This paper deals with automatic generation control of an interconnected two area thermal system. Appropriate generation rate constraint area considered in the areas. Performance of several classical controller like integral (I),proportional plus integral controller (PI),proportional plus integral plus derivative (PID) are compared with classical controller which are newly introduced in AGC named as proportional plus integral plus double derivative . And it will give better dynamics than other controller. Selection of suitable value of governors speed regulation parameter (R) has been examined.

Wen Tan, [3] PID tuning of load frequency controllers for power systems is discussed in this paper. The tuning method is based on two degree of freedom internal model control design method. The performance of the resulting PID controller is related to two tuning parameter thus detuning is easy when necessary. Unified PID tuning technique dependent on two degree-of-freedom for LFC of power system is discussed. Also time domain act in addition to robustness of consequential PID controller is associated to two regulation constraints as well as its robustness is discussed. Simulation results shows improvement in damping of power systems. The additional degree-of-freedom cancels the impact of unwanted poles of disturbance reduction performance of system having closed-up.

F.C. Tacker, T.W. Reddoch, O.T. Pan, and T. D. Linthon [4]: It has discussed the LFC of interconnected power system and investigated the formulation of LFC through linear control theory. So comparison between these was made to the ability for motivation of the transients (GRC) was introduced in these studies, considering both discrete and continuous power system.

C. Fosha, O.I. Elgerd [4]: This paper records the development of a state variable model of the megawatt – frequency control problem of multi area electric energy systems. For application of theorems of modem optimal control theory the model is represented in mathematical form that considered before is developed. The results of this study allow the authors to explain the ways of greatly improving dynamic response and stability margins of the megawatt – frequency control systems.

C. Concordia and L.K. Kirchmayer [6] in this paper they has discussed the first attempt in case of LFC has to control the power system frequency by the help of the governer. This technique of governor control was not sufficient for the stabilization of the system. So, an extra supplementary control technique was introduced to the governor by the help of a variable proportional directly to the deviation of frequency plus it's integral. This scheme contains classical approach of Load Frequency Control (LFC) of power system.

# 2. MATERIALS AND METHODS

# 2.1. Systems model

The multi-area power system consists of inter-connection of two unequal thermal systems as shown in Figure 1. Area-1 is having two units of thermal systems with reheater and area-2 having two units' thermal systems without reheater. Each area has three inputs and two outputs. The inputs are the controller inputs  $\Delta$ Pref, load disturbance  $\Delta$ PD, and tie-line power error  $\Delta$ Ptie.The outputs are the generator frequency  $\Delta$ F and area control error (ACE) given by, ACE=B $\Delta$ F+ $\Delta$ PTie, where B is the frequency bias parameter

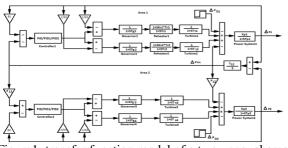


Figure1: transfer function model of a two unequal area thermal system.

## 2.2. System under study

Two unequal area thermal system of area capacity, Area1:2000MW, Area2:10000MW. While modelling interconnected areas of different capacities, a parametera12=-Pr1/Pr2are considered in the two area system. Different controller like proportional plus integral plus derivative (PID), Proportional plus integral plus derivative with structure1 (PID1), proportional plus integral plus derivative with structure 2 (PID2) are investigated separately. The nominal parameters of PID are taken form [2].

Simulations were conducted on an Intel, core i-5 core CPU, of 2.4 GHz and 4GB RAM computer in the MATLAB8.3.0.532 (R2014a; The math work, Natick, Massachusetts, USA) environment.

#### 2.3. Controller Structure

To control the frequency, PID/PID1/PID2 controllers are provided in each area. The structure 1and2of PID(PID1&PID2) controller are shown in fig.2(a) and 2(b), where KP,KI and KD are proportional, integral and derivative gains respectively.

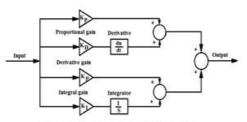


Figure 2 (a): Structure 1 of PID controller

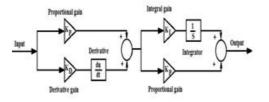


Figure 2(b): Structure 2 of PID controller

#### 3. RESULTS AND SIMULATIONS:

Table 1 shows different controller values of PID, PID structure 1 and PID structure 2 values

\$1.No.	Controller	Gain	Area 1	Area 2
1	PID	KP	1.9999	1.6150
		KI	1.9999	0.4390
		KD	0.7201	1.6449
2	PID 1	KP	1.7039	1.7789
		KI	1.9479	0.3080
		KD	1.9299	0.7699
		KP	1.9829	0.8520
3	PID 2	KP	2.0003	0.5579
		KI	1.9811	0.9341
		KD	1.7381	0.9120
		KP	2.0111	0.4169

3.1. Step increase in demand of area  $1(\Delta PD1)$ As the first test case, a step increase in load of 10% in area 1 is considered and the system dynamic response i.e. the frequency deviation of the area  $1(\Delta f1)$ ,the frequency deviation of area2 ( $\Delta f2$ ), tie line power deviation are shown

deviation of area2 ( $\Delta$ f2), tie line power deviation are shown in figures 3-5. It is clear from figures 3-5 that stability is improved and frequency error, tie-line power deviation gets reduced.

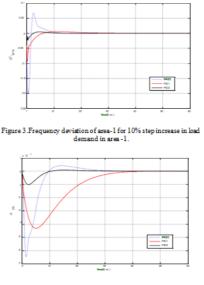


Figure 4. Frequency deviation of area-2 for 10% step increase in load demand in area -1.

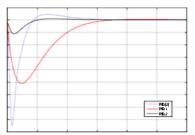


Figure 5.Tie-line power deviation for 10% step increase in load demand in area -1.

3.2. Step increase in demand of area  $2(\Delta PD2)$ 

In this case, a step increase in load of 10% in area 2 is considered and the system dynamic response i.e. the frequency deviation of area1, the frequency deviation of area2, tie line power deviation is shown in figures 6-8. From these figures it can be seen that the under shoot, over shoot are also reduced which improves the stability.

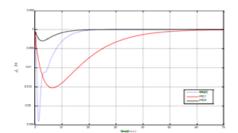


Figure 6. Frequency deviation of area-1 for 10% step increase in load demand in area -2.

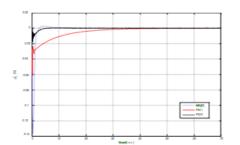


Figure 7. Frequency deviation of area-2 for 10% step increase in load demand in area -2.

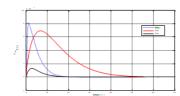


Figure 8. Tie-line power deviation for 10% step increase in load demand in seas -2

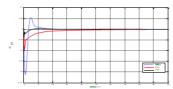


Figure 9. Frequency deviation of area-1 for 10% step increase in load demand in both areas.

3.3 Step increase in demand of the first and second area simultaneously

In this case a step increase in load of 10% in area 1 and area2 simultaneously are considered and system dynamic response is shown in figure(9-11) it is clear from figure(9-11) the best dynamic performance is obtained by PID structure 1 and PID structure 2 compared to the conventional PID controller in terms of settling times in frequency and tie-line power deviations.

Hence it can be concluded that the design structure 1 and structure 2 of PID controllers are robust perform satisfactorily under different operating condition.

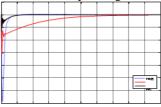


Figure 10.Frequency deviation of area-2 for 10% step increase in load demand in both areas.

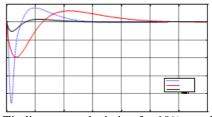


Figure 11.Tie-line power deviation for 10% step increase in load demand in both areas.

# **4. CONCLUSION**

In this paper, an attempt has been made to use different structure of Proportional plus Integral plus Derivative controllers (PID1&PID2) in AGC for two unequal area thermal system, which provides much better performances than conventional PID controller. Simulation result emphasis that the designed structured 1 and 2 of PID controller gives the better response and the system gets stable in terms of frequency deviation and tie line power deviation within shortest settling time. It has the potentiality of implementation in real time environment.

## **APPENDIX:**

The nominal parameters of the system investigated are as follows : Two-unequal –area thermal system F=60HZ,Pr1=2000MW,Pr2=10000MW,B1=0.4249, B2=0.4249,R1=2.4,R2=2.4,R3=2.4,R4=2.4,Tg1=0.08,Tg2=0.085,Tg3=0.085,Tg3=0.085,Tg4=0.085,Tt1=0.35,Tt2=o. 35,Tt3=0.35,Tt4=0.35,Kr1=0.5,Kr2=0.5,Tr1=10,Tr2=10,K p=120,T12=0.0866,Tp1=20,Tp2=20

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